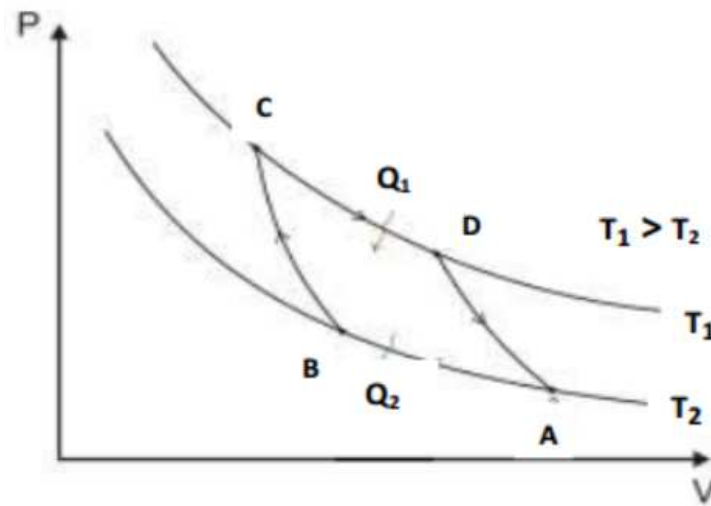


Tutorials. No. 1: Thermal Machines

Exercise 01: (Thermal motor/ refrigeration machine)

Part 1: Clapeyron (P-V) Diagram Representation



The described cycle includes:

- **AB (Isothermal Compression at T_2):** During isothermal processes, PV is constant. Since it's a compression, the volume decreases, so the curve approaches the origin on the P-V diagram, moving leftward.
- **BC (Adiabatic Compression):** Adiabatic processes do not exchange heat with the environment ($Q = 0$). The temperature increases as the gas is compressed. On a P-V diagram, this results in a steeper curve upwards.
- **CD (Isothermal Expansion at T_1):** Another isothermal process, but at a higher temperature T_1 where the volume increases, moving rightward on the P-V diagram while staying on the same isothermal curve.
- **DA (Adiabatic Expansion):** The gas expands without heat exchange. The volume increases, and the temperature decreases, curving back to the starting point.

Direction: The cycle moves clockwise, which is typical for heat engines (work is done by the system).

Sign of Work: Positive, as the system (engine) does work on the surroundings over one complete cycle.

Part 2: Volume Ratios

For adiabatic processes, $PV^\gamma = \text{constant}$ and $TV^{\gamma-1} = \text{constant}$, where $\gamma = C_P/C_V$ (specific heat ratio). From state B to C and D to A, we have:

$$\frac{V_B}{V_A} = \left(\frac{T_A}{T_B}\right)^{\frac{1}{\gamma-1}}$$
$$\frac{V_C}{V_D} = \left(\frac{T_D}{T_C}\right)^{\frac{1}{\gamma-1}}$$

Since $T_A = T_B$ (adiabatic return to initial temperature) and $T_C = T_D$, the equations simplify to:

$$\frac{V_B}{V_A} = \frac{V_C}{V_D}$$

This shows that $(V_A/V_B) = (V_D/V_C)$, indicating identical ratios for compression and expansion stages due to adiabatic reversibility.

Part 3: Heat Exchanged, Q_1 and Q_2

For the isothermal processes:

- **Isothermal Expansion at T_1 (CD):** $Q_1 = nRT_1 \ln \frac{V_D}{V_C}$
- **Isothermal Compression at T_2 (AB):** $Q_2 = nRT_2 \ln \frac{V_B}{V_A}$

Given that the ratio $\frac{V_A}{V_B} = \frac{V_D}{V_C}$:

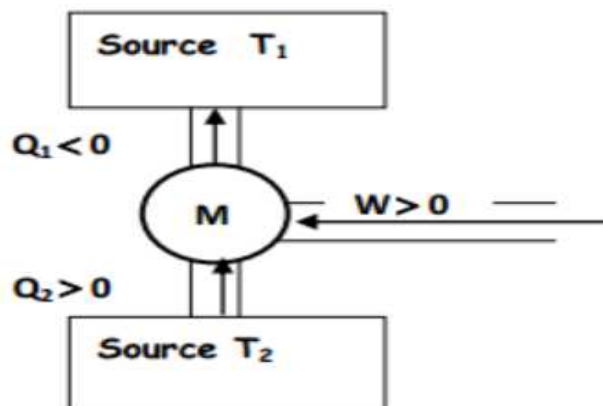
- $Q_2 = nRT_2 \ln \frac{V_A}{V_B}$
- Using Clausius equality, we deduce:

$$\frac{Q_1}{T_1} + \frac{Q_2}{T_2} = 0$$

Interpretation: The Clausius equality states that the net entropy change over a complete cycle is zero, confirming the reversibility of the cycle and conservation of energy in line with the Second Law of Thermodynamics.

Part 4: Refrigeration Machine Schematic

A refrigeration cycle involves extracting heat from a cold reservoir and expelling it to a hot reservoir by doing work on the system:



- **Heat extracted:** Q_2 from the cold reservoir.
- **Heat expelled:** Q_1 to the hot reservoir.
- **Work input:** To drive the compressor.

Part 5: Efficiency Calculation

For a refrigeration machine, the coefficient of performance (COP) is:

$$\text{COP} = \frac{|Q_2|}{W}$$

Given:

- $T_1 = 25^\circ\text{C} = 298\text{K}$
- $T_2 = -15^\circ\text{C} = 258\text{K}$

For ideal conditions:

$$\text{COP}_{\text{ideal}} = \frac{T_2}{T_1 - T_2} = \frac{258}{298 - 258} = \frac{258}{40} = 6.45$$

Part 6: Heat Extracted from Cold Source

Given:

- Work consumed = 12 kJ
- $\text{COP}_{\text{real}} = 6.45$ (using ideal as a reference)

$$Q_2 = \text{COP} \times W = 6.45 \times 12 \text{ kJ} = 77.4 \text{ kJ}$$

Conclusion: This calculation shows the cycle's feasibility as a refrigeration system, highlighting the energy efficiency and functionality in terms of heat transfer and work input.

Exercice: 2. Moteur Diesel.

1) Coordonnées des points B, C et D :

✓ Point B : A→B, transformation réversible adiabatique, $T_A V_A^{\gamma-1} = T_B V_B^{\gamma-1} \Rightarrow V_B = V_A \cdot \left(\frac{T_A}{T_B}\right)^{\frac{1}{\gamma-1}}$

A.N : $V_B = 0,16 \ell$.

De même on a : $T_A^\gamma P_A^{1-\gamma} = T_B^\gamma P_B^{1-\gamma} \Rightarrow P_B = P_A \cdot \left(\frac{T_A}{T_B}\right)^{\frac{\gamma}{1-\gamma}}$; A.N : $P_B = 44,3 \text{ atm}$.

✓ Point C : B→C, transformation isobare, $P_C = P_B = 44,3 \text{ atm}$.

De plus, loi des gaz parfaits ; $P_B V_B = n R \cdot T_B$ et $P_C V_C = n R \cdot T_C \Rightarrow T_C = \frac{V_C}{V_B} \cdot T_B$;

A.N : $T_C = 1431 \text{ K}$

✓ Point D : C→D, transformation réversible adiabatique, $T_C V_C^{\gamma-1} = T_D V_D^{\gamma-1} \Rightarrow T_D = T_C \cdot \left(\frac{V_C}{V_D}\right)^{\gamma-1}$;

A.N : $T_D = 569,7 \text{ K}$

De même on a : $P_C V_C^\gamma = P_D V_D^\gamma \Rightarrow P_D = P_C \cdot \left(\frac{V_C}{V_D}\right)^\gamma$; A.N : $P_D = 1,76 \text{ atm}$.

	A	B	C	D
P (atm.)	1,00	44,3	44,3	1,76
T (K)	323	954	1431	569,7
V (litre)	2,4	0,16	0,24	2,40

2) Allure du cycle décrit par le gaz dans le diagramme de Clapeyron :

3)

Nombre n de moles du gaz :

$$n = \frac{P_A V_A}{R T_A} ; \text{A.N : } n = 8,94 \cdot 10^{-2} \text{ mole}$$

$$\text{Ou } n = \frac{P_D V_D}{R T_D} ; \text{A.N : } n = 8,918 \cdot 10^{-2} \text{ mole}$$

Soit $n \approx 8,9 \cdot 10^{-2} \text{ mole}$

4) Capacités thermiques :

$$C_V = \frac{n \cdot R}{\gamma - 1} ; \text{A.N : } C_V = 1,86 \text{ J} \cdot \text{K}^{-1} \text{ et } C_P = \gamma \cdot C_V ; \text{AN : } C_P = 2,6 \text{ J} \cdot \text{K}^{-1}$$

5) Travaux et quantités de chaleurs échangés par le gaz au cours de chacune des transformations AB, BC, CD et DA.

✓ A→B, transformation réversible adiabatique : $Q_{AB} = 0$;

$$\text{De plus } \Delta U_{AB} = W_{AB} = C_V \cdot (T_B - T_A) ;$$

$$\text{A.N : } W_{AB} = 1,17 \text{ kJ}.$$

✓ B→C, transformation isobare : $Q_{BC} = C_P \cdot (T_C - T_B)$;

$$\text{A.N : } Q_{BC} = 1,24 \text{ kJ}.$$

$$\text{Et } W_{BC} = -P_B \cdot (V_C - V_B) ;$$

$$\text{A.N : } W_{BC} = -0,35 \text{ kJ}.$$

✓ C→D, transformation réversible adiabatique : $Q_{CD} = 0$

$$\text{Et } \Delta U_{CD} = W_{CD} = C_V \cdot (T_D - T_C) ;$$

$$\text{A.N : } W_{CD} = -1,6 \text{ kJ}.$$

✓ D→A, transformation isochore : $W_{DA} = 0$

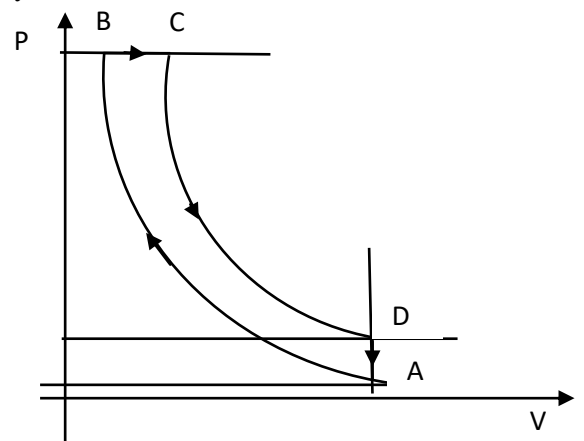
$$\text{De plus } \Delta U_{DA} = Q_{DA} = C_V \cdot (T_A - T_D) ;$$

$$\text{A.N : } Q_{DA} = -0,46 \text{ kJ}.$$

6) Rendement thermodynamique ρ du moteur Diesel étudié.

Par définition : $\rho = -\frac{W_{\text{cycle}}}{Q_C}$; avec Q_C étant la quantité de chaleur reçue par le moteur. Dans notre

cas $Q_C = Q_{BC} = 1,24 \text{ kJ}$. D'où :



$$\rho = - \frac{W_{cycle}}{Q_{BC}} = - \frac{W_{AB} + W_{BC} + W_{CD}}{Q_{BC}} ;$$

$$\text{A.N : } \rho = 0,63 = 63\%$$

7) Rendement d'un moteur de Carnot fonctionnant entre les mêmes températures extrêmes du cycle.

Les températures extrêmes du cycle sont T_A et T_C et par conséquent, le rendement de Carnot s'écrit :

$$\rho_{Carnot} = 1 - \frac{T_A}{T_C} = 0,77 = 77\%$$

8) $\rho_{Carnot} > \rho_{Diesel}$, le moteur Diesel est moins performant que le moteur de Carnot car ce dernier est idéal car formé de transformations réversibles.